# MATHEMATICAL MODELLING OF LOG NORMAL ATMOSPHERIC TURBULENCE CHANNELS 

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# of the Thesis: Mathematical Modelling of Log Normal Atmospheric Turbulence Channels 

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I certify that this thesis satisfies all the requirements as a thesis for the degree of Master of Science.


This is to certify that we have read this thesis and that in our opinion it is fully adequate, in scope and quality, as a thesis for the degree of Master of Science.


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## STATEMENT OF NON-PLAGIARISM PAGE

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ABSTRACT<br>Mathematical Modeling of Log Normal Turbulence Channels<br>GÖRSE, Serkan<br>M.Sc., Department of Electronic and Communication Engineering Supervisor: Assoc. Prof. Dr. Orhan GAZİ

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In this thesis work we demonstrated the development of a mathematical model for those systems involving complex numerical integration formulas. For this purpose, we considered two-hop communication systems. For the two-hop communication systems, the end-to-end performance depends on the harmonic mean of hop SNRs. For log-normal distributed channels, we considered two-hop communication systems and calculated the harmonic mean of two SNRs. The calculated harmonic mean value is in integral form and it need to be calculated numerically. We showed that such an integral formula can be expressed approximately using simple mathematical expressions. For this purpose, we used curve fitting utility of the MATLAB platform and approximated the harmonic mean expression by a Gaussian like distribution. Using the approximation formula, cumulative distribution function, moments generating function, moments, outage probability, amount of fading and transmission error probability are calculated in closed forms. The proposed approach presented in this thesis work can be used for the systems having long and complex performance calculation formulas.

Keywords: Performance of Free Space Optic, Harmonic Mean, Performance Analyses, Probability Density Function.

## öZ

# Log Normal Türbülans Kanallarının Matematiksel Modellemesi 

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Bu tez çalışmasında karmaşık numerik hesap gerektiren matematiksel bir denklemin daha basit ve kapalı formda olan matematiksel bir ifade ile yaklaşık olarak elde edilmesine yönelik bir çalışma sunulmaktadır. Bunun için iki atlamalı haberleşme sistemleri düşünülmüştür. İki atlamalı haberleşme sistemlerinin uçtan-uca olan performansları atlamalardaki SNR değerlerinin harmonik ortalamsına bağlıdır. Çalşsmamızda iki atlamalı ve Log-normal dağılımına sahip iletişim sistemlerinin atlama noktalarındaki SNR dağılımlarının harmonik ortalama değerini integral formunda hesapladık. Daha sonra hesaplamış olduğumuz integral formundaki karışık matematiksel ifadeyi MATLAB derleyicisinin curve-fitting aracın kullanarak daha basit matematiksel ifadelerle yaklaşık olarak hesapladık. Hesapladığımız yaklaşık değer formülü kapalı formdadır ve bu formülü kullanarak kümülatif dağılım fonksiyonu, moment üretim fonksiyonu, kesinti olasıllğı fonksiyonu, gönderim hata olasılığı gibi fonksiyonları kapalı formda hesapladık. Son olarak da hesapladığımız fonksiyonları kullanarak sistemin performansını gönderim hata olasılığı grafiği ile göstermiş olduk.

Anahtar Kelimeler: Serbest Uzay Optik Sistem Performansı, Harmonik Ortalama, Performans analizi, Olası yoğunluk fonksiyonu.

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## LIST OF ABBREVIATIONS

| FSO | Free Space Optics |
| :--- | :--- |
| PDF | Probability Density Function |
| SNR | Signal Noise Ratio |
| CDF | Cumulative Density Function |
| MGF | Moment Generating Function |
| BER | Bit Error Rate |

## CHAPTER 1

## INTRODUCTION

### 1.1 Background

In today's conditions, the need for more favorable opportunities, environment and tools in the communication world have increased. Every passing day, the necessity of optic communication systems is escalating in various areas such as telephone, networks data transmission, integrated optic mechanisms, cable television systems, transportation, military and medical applications in the direction of the abovementioned requirements. High speed data transmission speed for the optical networks is possible.

In present technology, the optical communication systems are more preferred than the other communication systems. Optical communication systems have some advantages over the classical communication systems, the existence of the silicium which is the raw material of the optical wave guide as a glut in the nature, stoutness of the isolation, the velocity head, stableness, being not affected by the electromagnetic effects, reliability, cost-efficiency and specifically having a large capacity and low transmission loss with high band width. The use of the optical fibers which are the dielectric transmission medium is increasing alongside the wired communication media such as the copper cable and coaxial cable. Because it has much less loss than the free space wireless communication. Its sufficiency to work in coordination with the old communication systems is one of the significant characteristic of optical fibers.

Free Space Optic (FSO) systems transmit data for telecommunications or computer networks. In contrast to the radio frequency networks, free space optical (FSO) communications provide many advantages which cause FSO to become increasingly popular and studied over the past decade. Most important advantages of FSO
communication systems are transmission rate, low cost, systematical, portability security and licensing. Free space optical systems use light propagation in free space. Free space means air, outer space or something similar. Today we use fiber optic cables for computer networks or high speed communication. Fiber optic cables cannot be useful when the physical connection is not possible. Systems which include fiber optic cables have high level cost in some places. For example, fiber deployment in urban areas could cost $\$ 300000-\$ 700000$ per kilometer without other installation cost. A FSO system with same transmission rate could be more economic at a price of $\$ 18000$ [4,5]. Although FSO systems can be a good solution to overcome these disadvantages, there are limitations as well. The degrading factors for optical communication include the fact that rain, dust, snow, fog or smog can obstruct the transmission path and these factors can shut down the network. Scientists try to improve FSO systems to avoid the air conditions that lead to limitations on communication systems. They develop many hardware and communication technique to overcome these difficulties.

### 1.2 Objectives

The main aim of this thesis is to develop a mathematical model for free space optic communication systems over log normal turbulence channels. There are many factors that affect the optical communication's system performance on atmosphere. Distance, temperature, altitude and pressure are some of important factors. Performance of FSO systems are analyzed by changing distance. These effects are demonstrated by graphs which are plotted by MATLAB in details. Cumulative density function, moments generating function, amount of fading and bit error rate are calculated.

### 1.3 Organization of the Thesis

This thesis is divided into four chapters. All analyses are studied to calculate performance of FSO channels over log normal turbulence channels. Results are compared with different distance and turbulence strength.

Chapter-1 covers an introduction and a background for free space optic's communication systems and portrays objectives of this thesis.

Chapter-2 involves the mathematical modeling of optic communication channels over log normal atmospheric turbulence channels.

Chapter-3 explains calculation of cumulative density function, moment generation function, moments, amount of fading and bit error rate with the mathematical model developed in Chapter-2.

Chapter-4 is the conclusion part.

## CHAPTER 2

## MATHEMATICAL MODELLING OF LOG NORMAL ATMOSPHERIC TURBULANCE CHANNELS

### 2.1 Probability Density Function of Log Normal Distribution

In this part of thesis, we work on the performance of FSO channels by investigating their outage probability and the average capacity, respectively. Thus, we derive closed form expressions for the outage probability and the average capacity of optical links over atmospheric turbulence induced fading channels modeled by the log normal turbulence distribution with respect to the turbulence strength, as well as the influence of other important system's parameters, such as optical link length and the receiver's aperture diameter.

Firstly, we calculate the probability density function by utilizing the harmonic mean of two signals. Given two numbers $X_{1}$ and $X_{2}$, the harmonic means of $X_{1}$ and $X_{2}$, is defined as $[6,9]$

$$
\begin{equation*}
\mu_{H}\left(X_{1}, X_{2}\right)=\frac{2 X_{1} X_{2}}{X_{1}+X_{2}} \tag{2.1}
\end{equation*}
$$

We define three parameters ( $x z w$ ) to express this equation more easily. These parameters are equal to

$$
\begin{equation*}
w=X_{1}+X_{2} \quad z=2 X_{1} X_{2} \quad x=\frac{z}{w} \tag{2.2}
\end{equation*}
$$

For the harmonic mean calculation of two random variables, we consider the random variables having log-normal distribution. The probability density function equation of the log normal turbulence as given by

$$
\begin{equation*}
p(x)=\frac{1}{2 \mu \sigma \sqrt{2 \pi}} \exp \left(-\frac{\left(\ln \left(\frac{\mu}{\bar{\mu}}\right)+\sigma^{2}\right)^{2}}{8 \sigma^{2}}\right) \tag{2.3}
\end{equation*}
$$

where $\sigma$ is the standard deviation of the log normal distribution, which depends on the channel's characteristics and it is calculated as [9, 17]

$$
\begin{equation*}
\sigma^{2}=\exp \left[\frac{0.49 \delta^{2}}{\left(1+0.18 d^{2}+0.56 \delta^{\frac{12}{5}}\right)^{\frac{7}{6}}}+\frac{0.51 \delta^{2}}{\left(1+0.9 d^{2}+0.62 d^{2} \delta^{\left(\frac{12}{5}\right)}\right)^{\frac{5}{6}}}\right]-1 \tag{2.4}
\end{equation*}
$$

where

$$
d=\sqrt{\frac{k D^{2}}{4 L}}
$$

and

$$
k=\frac{2 \pi}{\lambda}
$$

is the optical wave number, $L$ is the length of the optical link and $D$ is the receiver's aperture diameter. The parameter $\delta$ is called Rytov variance and it is defined as

$$
\begin{equation*}
\delta^{2}=1.23 C_{n}^{2} k^{\frac{7}{6}} L^{\frac{11}{6}} \tag{2.5}
\end{equation*}
$$

where $C_{n}^{2}$ is the altitude which is dependent on the turbulence strength varying from $10^{-17}$ to $10^{-13} \mathrm{~m}^{-2 / 3}$ according to atmospheric turbulence conditions [2,8].The instantaneous electrical signal to noise ratio (SNR) is given as

$$
\mu=\left(\frac{\eta I^{2}}{N_{0}}\right)=\frac{s^{2}}{N_{0}}
$$

and the average electrical SNR is calculated as

$$
\bar{\mu}=\eta \frac{E[I]}{N_{0}} .
$$

Now we must use error function to define $p d f$ equation of log normal model more simply.
The exponential term in log-normal distribution in (2.3) can be expressed as in

$$
\begin{equation*}
p(x)=\exp \left(-\frac{\left(\ln \left(\frac{\mu}{\bar{\mu}}\right)+\sigma^{2}\right)^{2}}{8 \sigma^{2}}\right) \rightarrow \exp \left[-\left(\frac{1}{8 \sigma^{2}}\right)\left[\ln \left(\frac{\mu}{\bar{\mu}}\right)\right]^{2}+\sigma^{4}+2 \sigma^{2} \ln \left(\frac{\mu}{\bar{\mu}}\right)\right] . \tag{2.6}
\end{equation*}
$$

After this operation, probability density functions of log normal distribution take the form

$$
\begin{equation*}
p(x)=\frac{1}{2 \sigma \sqrt{2 \pi}} \exp \left[-\frac{\sigma^{2}}{8}\right] \bar{\mu}^{-\left(\frac{1}{4}\right)} \mu^{\frac{1}{4}} \exp \left[-\left(\frac{1}{8 \sigma^{2}}\right)\left[\ln \left(\frac{\mu}{\bar{\mu}}\right)\right]^{2}\right] . \tag{2.7}
\end{equation*}
$$

If we define the constant value $K$ as in

$$
\begin{equation*}
K=\frac{1}{2 \sigma \sqrt{2 \pi}} \exp \left[-\frac{\sigma^{2}}{8}\right] \bar{\mu}^{-\left(\frac{1}{4}\right)} \tag{2.8}
\end{equation*}
$$

then the log-normal distribution in (2.7) can be written as in (2.9)

At the end of these steps pdf equation transformed to an easier form which is expressed as equation(2.9).

$$
\begin{equation*}
p(x)=K \cdot \mu^{\frac{1}{4}} \cdot \exp \left[\left[\ln \left(\frac{\mu}{\bar{\mu}}\right)\right]^{2}\right] \tag{2.9}
\end{equation*}
$$

### 2.2 Joint Probability Density Function

The joint pdf of the random variables $Z, W$, i.e., $P_{z, w}(z, w)$ can be derived using the Jacobian transformation. We can write the harmonic mean of $X_{1}$ and $X_{2}$ as $X=$ $Z / W$ where $X=2 X_{1} X_{2}$ and $W=X_{1}+X_{2}$. Using [12, Sec. 6.2], the PDF of $X$ can be written as,

$$
\begin{equation*}
p_{x}(x)=\int_{-\infty}^{\infty}|w| P_{z, w}(x w, w) d w \tag{2.10}
\end{equation*}
$$

which can be evaluated with the help of [7, Eq. (3.383.4)] yielding,

$$
\begin{equation*}
P_{z, w}=\frac{1}{2 \Delta}\left[P_{x_{1}, x_{2}}\left(X_{11}, X_{21}\right), P_{x_{1}, x_{2}}\left(X_{12}, X_{22}\right)\right] \tag{2.11}
\end{equation*}
$$

in which we have

$$
\begin{equation*}
X_{11}, X_{21}=w \pm \frac{\sqrt{w^{2}-2 z}}{2}, X_{11}, X_{21}=w \pm \frac{\sqrt{w^{2}-2 z}}{2}, \Delta=\sqrt{w^{2}-2 z} \tag{2.12}
\end{equation*}
$$

Substituting the parameters in (2.11), and the log-normal distribution expression in (2.9) into we obtain (2.14).

$$
\begin{equation*}
P_{z, w}(z, w)=\frac{1}{2 \sqrt{w^{2}-2 z}}\left[P\left(x_{11}\right) P\left(x_{21}\right)+P\left(x_{12}\right) P\left(x_{22}\right)\right] \tag{2.13}
\end{equation*}
$$

$$
P_{z, w}(z, w)=\frac{2}{2 \sqrt{w^{2}-2 z}}\left[\begin{array}{l}
K\left(\frac{(w+\Delta)}{2}\right)^{\frac{1}{4}} \exp \left(\frac{1}{8 \sigma^{2}}\left[\ln \left(\frac{(w+\Delta)}{2} \frac{1}{x}\right)\right]^{2}\right)  \tag{2.14}\\
K\left(\frac{(w-\Delta)}{2}\right)^{\frac{1}{4}} \exp \left(\frac{1}{8 \sigma^{2}}\left[\ln \left(\frac{(w-\Delta)}{2} \frac{1}{x}\right)\right]^{2}\right)
\end{array}\right] .
$$

The probability density function of $X=Z / W$ can be calculated using

$$
P_{X}(x)=\int_{2 x}^{\infty} w P_{z, w}(x w, w) d w
$$

leading to

$$
\begin{equation*}
p(x)=K \int_{2 x}^{\infty} w^{-\left(\frac{3}{4}\right)}(w-2 x)^{-\left(\frac{1}{2}\right)} \exp \left(-\frac{1}{8 \sigma^{2}}\left[\left[\frac{w+\Delta}{2 a}\right]^{2}\left[\frac{w-\Delta}{2 a}\right]^{2}\right]\right) d w . \tag{2.15}
\end{equation*}
$$

This integration is cannot be expressed in closed form. We write some code in MATLAB to calculate this integral and we plot its graph vs. SNR, i.e., vs. $x$. The graph of this $p(x)$ is shown on Fig. 1 .


Figure 1 Probability Density Function to Signal Noise Ratio

### 2.3 Detection of Best Fitting Curves in MATLAB

MATLAB curve fitting option is used to find the best mathematical expression that approximates the probability density function in (2.15) closely. To express the integration defined in (2.15) in closed form, different curve fitting models of the MATLAB can be utilized. The typical curve fitting models available in MATLAB are Gaussian, Fourier, and Polynomial. We decide for Gaussian model with $1^{\text {st }}$ degree. Because, we obtain best fitting performance and simple integration in Gaussian model. Performance analysis and coefficients values of Gaussian model are shown in Fig. 2, Fourier model is shown in Fig. 3 and Polynomial model is shown in Fig. 4. At the same time, we compare the number of terms, general mode of equation, goodness of fit and coefficient values in Fig. 2, 3 and 4.


Figure 2 Gaussian Equation Model


Figure 3 Polynomial Equation Model


Figure 4 Fourier Equation Model

After we decide on the $1^{\text {st }}$ degree Gaussian equation, instead of the complex $p(x)$ integral equation we use the Gaussian equation obtained from curve fitting utility of the MATLAB. That is, $p(x)$ in (2.15) is closely approximated by

$$
\begin{equation*}
p(x)=A * \exp \left(-\left(\frac{(X-B)}{C}\right)^{2}\right) \tag{2.16}
\end{equation*}
$$

Thus using (2.16), we can calculate $p(x)$ more easily than complex integration form defined in equation (2.15). In the simple equation in (2.16), we have some coefficients $A, B, C$. We calculate these coefficients using MATLAB in the next part of thesis.

### 2.4 Coefficient Analyze According to Distance

In pursuit of this process we concentrate on the changes of $A, B, C$ when we change distance $L$. In order to see this, we wrote a MATLAB code. The range value for $L$ is 500 m to 2500 m , and for each $L$ value, we calculate the $A, B, C$ coefficients. After that, we plot the graphs of $A, B, C$ with respect to $L$ as indicated in Fig. 5, Fig. 6 and Fig. 7.


Figure 5 Change of $A$ with respect to $L$


Figure 6 Change of $B$ with respect to $L$


Figure 7 Change of $C$ with respect to $L$
we inspect the change of the coefficients with distance. When we look at the results, $A$ and $C$ are increasing with distance but $B$ is increasing until nearly 1500 meter. This means that the best distance is between 1000 and 1500 meter for our model. In next stage, we analyze how coefficients change with turbulence strength $\mathrm{Cn}^{2}$ whose value depends on the $\sigma$ variable in equation (2.5).

### 2.5 Coefficient Analyze According to Turbulence Strength

In this section, we inspect the change of $A, B, C$ with $C n^{2}$ which is the altitude dependent turbulence strength varying from $10^{-17}$ to $10^{-13} \mathrm{~m}^{-2 / 3}$ according to the atmospheric turbulence conditions. Fifty different $\mathrm{Cn}^{2}$ values ranging from $1.7 \times 10^{-14}$ to $1.7 \times 10^{-13.5}$ are employed. We plot graph of to $A, B, C$ with respect to $\mathrm{Cn}^{2}$ as in Fig.8, Fig. 9 and Fig. 10.


Figure 8 Change of A with respect to $\mathrm{Cn}^{2}$


Figure 9 Change of B with respect to $\mathrm{Cn}^{2}$


Figure 10 Change of C with respect to $\mathrm{Cn}^{2}$

These graphs in Fig. 8, Fig. 9 and Fig. 10 mean that coefficient values increase in a regular manner when $\mathrm{Cn}^{2}$ increases. This indicates that it is possible to relate the changes in the coefficients to the $\mathrm{Cn}^{2}$ using the curve fitting utility of the MATLAB platform. In Table. 1 and Table 2, the coefficient values for different values of $\mathrm{Cn}^{2}$ are tabulated.

We also inspect the change of the coefficients with regard to the changes in $\mathrm{Cn}^{2}$ and $L$. We use $50 \mathrm{Cn}^{2}$ values ranging from $1.7 \times 10^{-14}$ to $1.7 \times 10^{-13.5}$. The $L$ values are chosen from 500 m to 2500 m . We implemented MATLAB's curve fitting options to these graphs. We detected best fitting option which is polynomial fitting in $6^{\text {th }}$ degree for these graphs. After this fitting process, every graph is expressed via a polynomial equation in the form

$$
\begin{equation*}
p_{1} X^{6}+p_{2} X^{5}+p_{3} X^{4}+p_{4} X^{3}+p_{5} X^{2}+p_{6} X^{1}+p_{7} \tag{2.17}
\end{equation*}
$$

|  | $C^{\wedge} 12=1.7000 \mathrm{e}-14$ |  |  | $\underline{C n^{\wedge} 2=1.7750 e-14}$ |  |  | $\underline{C n^{\wedge} 2=1.8500 e-14}$ |  |  | $\underline{\mathrm{C}^{\wedge} 2=1.9251 e-14}$ |  |  | $\underline{C n^{\wedge} 2=2.0001 e-14}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 |
| P1 | -0.01664 | 0.006776 | 0.005109 | 0.142 | 0.005455 | 0.003926 | 0.3267 | 0.003664 | 0.002459 | 0.5338 | 0.001471 | 0.0007687 | 0.7585 | -0.00104 | -0.001076 |
| $\underline{p}$ | -2.035 | 0.02323 | 0.01297 | -2.171 | 0.02663 | 0.01493 | -2.258 | 0.02963 | 0.01655 | -2.291 | 0.03216 | 0.01781 | -2.265 | 0.03415 | 0.0187 |
| $\underline{\text { P3 }}$ | -1.327 | -0.04495 | -0.02925 | -2.576 | -0.03472 | -0.02191 | -3.949 | -0.02203 | -0.01317 | -5.419 | -0.00725 | -0.00336 | -6.953 | 0.009148 | 0.007177 |
| P4 | 21.46 | -0.2162 | -0.0873 | 22.29 | -0.2368 | -0.09648 | 22.85 | -0.2551 | -0.1041 | 23.13 | -0.2709 | -0.11 | 23.12 | -0.2839 | -0.1142 |
| $\underline{\text { p5 }}$ | 67.97 | 0.1561 | 0.1826 | 75.2 | 0.1196 | 0.1702 | 82.58 | 0.07893 | 0.1559 | 90.05 | 0.03498 | 0.1402 | 97.53 | -0.01146 | 0.1237 |
| $\underline{\text { P6 }}$ | 115.6 | 0.562 | 4.316 | 126.3 | 0.5887 | 4.434 | 137.7 | 0.6106 | 4.548 | 149.5 | 0.6276 | 4.658 | 161.9 | 0.6399 | 4.765 |
| $\underline{\text { P7 }}$ | 96.62 | 17.68 | 9.132 | 103.3 | 17.72 | 9.374 | 110.2 | 17.75 | 9.613 | 117.5 | 17.78 | 9.848 | 125.1 | 17.81 | 10.08 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $\underline{C N \wedge}$ ^2.0751e-14 |  |  | $\underline{C N}{ }^{\wedge}=2.1501 e-14$ |  |  | $\underline{C n^{\wedge} 2=2.2251 e-14}$ |  |  | $\underline{C N A 2}=2.3001 e-14$ |  |  | $\underline{C n^{\wedge} 2=2.3752 e-14}$ |  |  |
|  | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 |
| $\underline{P 1}$ | 0.9967 | -0.003789 | -0.003016 | 1.244 | -0.006694 | -0.004993 | 1.496 | -0.009676 | -0.006957 | 1.75 | -0.01266 | -0.008864 | 2.001 | -0.0156 | -0.01068 |
| $\underline{P 2}$ | -2.177 | 0.03559 | 0.0192 | -2.026 | 0.03646 | 0.01932 | -1.81 | 0.03677 | 0.01908 | -1.531 | 0.03653 | 0.0185 | -1.187 | 0.03577 | 0.01761 |
| P3 | -8.519 | 0.02675 | 0.01814 | -10.09 | 0.04513 | 0.02926 | -11.63 | 0.0639 | 0.04027 | -13.13 | 0.0827 | 0.05096 | -14.54 | 0.1012 | 0.06116 |
| $\underline{P 4}$ | 22.82 | -0.2942 | -0.1167 | 22.26 | -0.3016 | -0.1175 | 21.43 | -0.3063 | -0.1169 | 20.35 | -0.3084 | -0.1147 | 19.04 | -0.308 | -0.1113 |
| P5 | 105 | -0.0597 | 0.1067 | 112.4 | -0.1091 | 0.08972 | 119.6 | -0.159 | 0.073 | 126.7 | -0.2089 | 0.05686 | 133.6 | -0.2584 | 0.04151 |
| $\underline{\text { P6 }}$ | 174.7 | 0.6476 | 4.868 | 188 | 0.6508 | 4.968 | 201.7 | 0.6498 | 5.064 | 215.7 | 0.6448 | 5.158 | 230.1 | 0.6361 | 5.249 |
| $\underline{\underline{P 7}}$ | 132.9 | 17.84 | 10.31 | 141.1 | 17.87 | 10.53 | 149.6 | 17.9 | 10.75 | 158.4 | 17.93 | 10.96 | 167.5 | 17.96 | 11.18 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $C^{\wedge}{ }^{\wedge}=2.4502 e-14$ |  |  | $\underline{C n^{\wedge} 2=2.5252 e-14}$ |  |  | $\underline{C n^{\wedge} 2=2.6002 e-14}$ |  |  | $\underline{C n^{\wedge} 2=2.6752 e-14}$ |  |  | $\underline{C n^{\wedge} 2=2.7502 e-14}$ |  |  |
|  | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 |
| $\underline{\text { P1 }}$ | 2.247 | -0.01842 | -0.01237 | 2.485 | -0.02107 | -0.01391 | 2.713 | -0.02353 | -0.01528 | 2.931 | -0.02575 | -0.01647 | 3.136 | -0.02772 | -0.01748 |
| $\underline{P 2}$ | -0.7806 | 0.03453 | 0.01643 | -0.3125 | 0.03284 | 0.01499 | 0.2161 | 0.03075 | 0.01332 | 0.8039 | 0.02829 | 0.01145 | 1.45 | 0.02551 | 0.00941 |
| $\underline{\text { P3 }}$ | -15.86 | 0.1192 | 0.0707 | -17.05 | 0.1363 | 0.07947 | -18.11 | 0.1525 | 0.08739 | -19.02 | 0.1675 | 0.09438 | -19.77 | 0.1813 | 0.1004 |
| P4 | 17.53 | -0.3053 | -0.1066 | 15.83 | -0.3005 | -0.101 | 13.97 | -0.2937 | -0.09434 | 11.97 | -0.2851 | -0.08693 | 9.855 | -0.2749 | -0.07886 |
| $\underline{\text { P5 }}$ | 140.2 | -0.3069 | 0.02718 | 146.6 | -0.3541 | 0.01401 | 152.7 | -0.3999 | 0.002096 | 158.6 | -0.4439 | -0.008482 | 164.2 | -0.486 | -0.01768 |
| $\underline{\text { P6 }}$ | 244.7 | 0.6238 | 5.338 | 259.6 | 0.6084 | 5.424 | 274.7 | 0.59 | 5.508 | 290.1 | 0.5689 | 5.59 | 305.6 | 0.5454 | 5.671 |
| $\underline{\text { P7 }}$ | 176.9 | 17.98 | 11.39 | 186.6 | 18.01 | 11.59 | 196.5 | 18.03 | 11.8 | 206.7 | 18.05 | 12 | 217.2 | 18.07 | 12.19 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | $\underline{C^{\wedge} 2=2.8253 e-14}$ |  |  | $\underline{C n^{\wedge} 2=2.9003 e-14}$ |  |  | $\underline{C n^{\wedge} 2=2.9753-14}$ |  |  | $\underline{C N}{ }^{\wedge}=3.0503 \mathrm{e}-14$ |  |  | $\underline{C n^{\wedge} 2=3.1253 e-14}$ |  |  |
|  | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 |
| $\underline{\text { P1 }}$ | 3.33 | -0.02943 | -0.0183 | 3.511 | -0.03085 | -0.01892 | 3.682 | -0.03199 | -0.01936 | 3.842 | -0.03284 | -0.01961 | 3.994 | -0.0334 | -0.01968 |
| $\underline{\text { P2 }}$ | 2.153 | 0.02245 | 0.007222 | 2.913 | 0.01915 | 0.004919 | 3.728 | 0.01567 | 0.00252 | 4.599 | 0.01202 | 4.954e-05 | 5.527 | 0.008246 | -0.002473 |
| $\underline{\text { p3 }}$ | -20.35 | 0.1938 | 0.1055 | -20.74 | 0.2048 | 0.1095 | -20.95 | 0.2145 | 0.1126 | -20.96 | 0.2227 | 0.1147 | -20.79 | 0.2295 | 0.1158 |
| P4 | 7.641 | -0.2633 | -0.07022 | 5.36 | -0.2505 | -0.06115 | 3.03 | -0.2366 | -0.05176 | 0.6708 | -0.2218 | -0.04213 | -1.697 | -0.2063 | -0.03236 |
| $\underline{\text { P5 }}$ | 169.5 | -0.5261 | -0.02548 | 174.4 | -0.564 | -0.03187 | 179.2 | -0.5997 | -0.03687 | 183.6 | -0.6333 | -0.04052 | 187.8 | -0.6646 | -0.04285 |
| $\underline{\text { P6 }}$ | 321.2 | 0.5196 | 5.749 | 336.9 | 0.4918 | 5.827 | 352.8 | 0.4621 | 5.903 | 368.7 | 0.4309 | 5.977 | 384.6 | 0.3982 | 6.051 |
| $\underline{\text { P7 }}$ | 227.9 | 18.09 | 12.39 | 238.8 | 18.1 | 12.58 | 250 | 18.12 | 12.77 | 261.4 | 18.13 | 12.96 | 273 | 18.14 | 13.14 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Table 1 Constant Values for 50 Pieces of $\mathrm{Cn}^{2}$

|  | CM ${ }^{\text {¢ } 2=3.5754 e-14}$ |  |  | $\underline{\operatorname{cn}}{ }^{2}=3.6505 \mathrm{e}-14$ |  |  | $\underline{C^{\wedge} 2=3.7255 e-14}$ |  |  | $\underline{C N A} 2=3.8005 \mathrm{e}-14$ |  |  | $\underline{C n^{\wedge} 2=3.8755 e-14}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 |
| P1 | 4.903 | -0.03135 | -0.01688 | 5.093 | -0.03022 | -0.01597 | 5.308 | -0.02891 | -0.01495 | 5.556 | -0.02743 | -0.01385 | 5.845 | -0.02581 | -0.01266 |
| P2 | 12.42 | -0.01532 | -0.01776 | 13.83 | -0.01919 | -0.02021 | 15.33 | -0.02298 | -0.02259 | 16.93 | -0.02669 | -0.02491 | 18.65 | -0.0303 | -0.02716 |
| P3 | -15.77 | 0.2427 | 0.1049 | -14.31 | 0.2408 | 0.1006 | -12.69 | 0.238 | 0.09559 | -10.92 | 0.2343 | 0.09006 | -9.008 | 0.2297 | 0.08402 |
| $\underline{P 4}$ | -15.16 | -0.1041 | 0.02506 | -17.17 | -0.08648 | 0.03387 | -19.08 | -0.06895 | 0.04232 | -20.89 | -0.05155 | 0.05039 | -22.6 | -0.03431 | 0.05804 |
| P5 | 208 | -0.8084 | -0.03265 | 210.7 | -0.8256 | -0.02756 | 213.3 | -0.8411 | -0.02169 | 215.9 | -0.855 | -0.01512 | 218.4 | -0.8673 | -0.007923 |
| P6 | 480.7 | 0.1806 | 6.474 | 496.7 | 0.1418 | 6.542 | 512.7 | 0.1027 | 6.609 | 528.6 | 0.0633 | 6.676 | 544.5 | 0.0236 | 6.743 |
| ${ }^{\text {P7 }}$ | 346.4 | 18.19 | 14.2 | 359.2 | 18.19 | 14.37 | 372.1 | 18.2 | 14.54 | 385.2 | 18.2 | 14. | 398.3 | 18.2 | 14.87 |
|  | C ${ }^{\wedge} 12=3.9505 \mathrm{e}-14$ |  |  | $\operatorname{cin}^{\wedge} 2=4.0256 \mathrm{e}-14$ |  |  | $\mathrm{Cn}^{\wedge} 2=4.1006 \mathrm{e}-14$ |  |  | C $\boldsymbol{M}^{\wedge} 2=4.1756 e-14$ |  |  | $\mathrm{Cn}^{\wedge} 2=4.2506 \mathrm{e}-14$ |  |  |
|  | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 |
| $\underline{P 1}$ | 6.183 | -0.02404 | -0.0114 | 6.58 | -0.02214 | -0.01008 | 7.048 | -0.02014 | -0.008702 | 7.598 | -0.01805 | -0.007279 | 8.243 | -0.01588 | -0.005807 |
| $\underline{P}$ | 20.48 | -0.0338 | -0.02933 | 22.46 | -0.03719 | -0.03143 | 24.59 | -0.04046 | -0.03343 | 26.89 | -0.04359 | -0.03534 | 29.39 | -0.0466 | -0.03714 |
| $\underline{\text { P3 }}$ | -6.97 | 0.2244 | 0.07752 | -4.814 | 0.2183 | 0.0706 | -2.562 | 0.2117 | 0.06329 | -0.2288 | 0.2045 | 0.05565 | 2.168 | 0.1968 | 0.04766 |
| P4 | -24.22 | -0.01729 | 0.06525 | -25.74 | -0.0005246 | 0.07201 | -27.18 | 0.01594 | 0.07826 | -28.54 | 0.03207 | 0.08401 | -29.83 | 0.04788 | 0.0892 |
| P5 | 220.8 | -0.8782 | -0.000173 | 223.2 | -0.8877 | 0.008073 | 225.7 | -0.896 | 0.01674 | 228.2 | -0.9031 | 0.02576 | 230.7 | -0.909 | 0.03511 |
| $\underline{p 6}$ | 560.4 | -0.01629 | 6.809 | 576.3 | $-0.05636$ | 6.874 | 592.2 | -0.09645 | 6.94 | 608.1 | -0.1366 | 7.005 | 624 | -0.1767 | 7.069 |
| P7 | 411.6 | 18.2 | 15.03 | 425 | 18.2 | 15.19 | 438.4 | 18.19 | 15.35 | 452 | 18.19 | 15.51 | 465.6 | 18.19 | 15.66 |
|  | Cn^2=4.3256e-14 |  |  | $\underline{C^{\wedge} 2=4.4006 e-14}$ |  |  | $\underline{C n^{\wedge} 2=4.4757 e-14}$ |  |  | $\underline{C N}{ }^{\wedge} \mathbf{2}=4.5507 e-14$ |  |  | $\underline{C N}{ }^{\text {2 } 2=4.6257 e-14}$ |  |  |
|  | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 |
| $\underline{p 1}$ | 9.001 | -0.01365 | -0.004319 | 9.886 | -0.01136 | -0.002802 | 10.92 | -0.009023 | -0.001259 | 12.12 | -0.006664 | 0.0002957 | 13.52 | -0.004286 | 0.00186 |
| P2 | 32.1 | -0.04946 | -0.03886 | 35.06 | -0.05218 | -0.04048 | 38.3 | -0.05477 | -0.042 | 41.83 | -0.05721 | -0.04341 | 45.72 | -0.05951 | -0.04471 |
| P3 | 4.604 | 0.1887 | 0.03946 | 7.057 | 0.1802 | 0.03101 | 9.502 | 0.1714 | 0.02233 | 11.9 | 0.1624 | 0.01349 | 14.22 | 0.1531 | 0.004511 |
| P4 | -31.09 | 0.0633 | 0.09391 | -32.32 | 0.07833 | 0.09806 | -33.56 | 0.09299 | 0.1017 | -34.84 | 0.1072 | 0.1047 | -36.2 | 0.1211 | 0.1071 |
| P5 | 233.4 | -0.914 | 0.04466 | 236.3 | -0.9179 | 0.0544 | 239.4 | -0.9211 | 0.06429 | 242.6 | -0.9233 | 0.07424 | 246.2 | -0.9249 | 0.08421 |
| $\underline{p}$ | 639.9 | -0.2167 | 7.133 | 655.9 | -0.2566 | 7.197 | 672 | -0.2965 | 7.261 | 688.1 | -0.3361 | 7.324 | 704.3 | -0.3756 | 7.387 |
| P7 | 479.3 | 18.18 | 15.82 | 493.1 | 18.17 | 15.97 | 507 | 18.17 | 16.12 | 520.9 | 18.16 | 16.27 | 534.8 | 18.15 | 16.42 |
|  | $\underline{\text { Cn }}$ 2 $=4.7007 \mathrm{e}-14$ |  |  | $\underline{C N A 2} 4.7757 \mathrm{e}-14$ |  |  | $\underline{C n^{\wedge} 2=4.8507 e-14}$ |  |  | $\underline{C^{\wedge} 2=4.9258 e-14}$ |  |  | Cn ${ }^{\text {2 } 2=5.0008 e-14}$ |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 | a1 | b1 | c1 |
| $\underline{P 1}$ | 15.13 | -0.001898 | 0.003429 | 17 | 0.0004902 | 0.004999 | 19.15 | 0.002871 | 0.006564 | 21.62 | 0.005239 | 0.008125 | 24.47 | 0.007589 | 0.009664 |
| $\underline{P}$ | 49.99 | -0.06166 | -0.04591 | 54.69 | -0.06367 | -0.047 | 59.88 | -0.06554 | -0.04799 | 65.63 | -0.06728 | -0.04887 | 71.99 | -0.06887 | -0.04965 |
| $\underline{P}$ | 16.41 | 0.1437 | -0.004591 | 18.44 | 0.1341 | -0.01379 | 20.25 | 0.1245 | -0.02305 | 21.77 | 0.1149 | -0.03238 | 22.93 | 0.1052 | -0.0417 |
| $\underline{P 4}$ | -37.68 | 0.1345 | 0.109 | -39.35 | 0.1475 | 0.1103 | -41.27 | 0.16 | 0.1111 | -43.51 | 0.1722 | 0.1113 | -46.15 | 0.184 | 0.1109 |
| P5 | 250.1 | -0.9257 | 0.09417 | 254.4 | -0.926 | 0.1041 | 259.1 | -0.9256 | 0.1139 | 264.2 | -0.9248 | 0.1235 | 270 | -0.9234 | 0.133 |
| $\underline{p 6}$ | 720.7 | -0.4149 | 7.449 | 737.2 | -0.4539 | 7.512 | 754 | -0.4927 | 7.574 | 770.9 | -0.5313 | 7.636 | 788.2 | -0.5696 | 7.697 |
| P7 | 548.8 | 18.14 | 16.57 | 562.9 | 18.14 | 16.72 | 577 | 18.13 | 16.86 | 591.1 | 18.12 | 17.01 | 605.2 | 18.1 | 17.15 |
|  |  |  |  |  |  |  | $\underline{C n^{\prime} 2=5.2258 e-14}$ |  |  |  |  |  |  |  |  |
|  | Cn^2=5.0758e-14 |  |  | $\underline{C N \wedge}$ |  |  |  |  |  | $\underline{C^{\prime} 2} \mathbf{2} 5.3009 \mathrm{e}-14$ |  |  | $\underline{C^{\wedge} 2=5.3759 e-14}$ |  |  |
| P1 | ${ }_{27}{ }^{\text {a }}$ | ${ }_{0}^{\text {b1 }}$ | ${ }^{\text {c1 }}$ | ${ }_{31}{ }^{\text {a }}$ | ${ }_{\text {b1 }} 0.01218$ | ${ }^{\text {c1 }}$ | ${ }^{\text {a }} 35$ | ${ }^{\text {b1 }}$ | ${ }_{0}^{\text {c1 }}$ | ${ }^{\text {a }} 10.61$ | b1 0.01659 | ${ }^{\text {c1 }}$ | a1 46 | b1 0.01873 | ${ }_{0.01716}$ |
| P2 | 79.04 | -0.07033 | -0.05031 | 86.87 | -0.07167 | -0.05086 | 95.58 | -0.07288 | -0.05131 | 105.3 | -0.07397 | -0.05166 | 116.1 | -0.07493 | -0.0519 |
| $\underline{\text { P3 }}$ | 23.65 | 0.09555 | -0.05105 | 23.83 | 0.08598 | -0.06039 | 23.37 | 0.0765 | -0.0697 | 22.13 | 0.06715 | -0.07901 | 19.98 | 0.05791 | -0.08821 |
| P4 | -49.31 | 0.1953 | 0.11 | -53.08 | 0.2063 | 0.1084 | -57.62 | 0.2169 | 0.1064 | -63.08 | 0.2271 | 0.1037 | -69.63 | 0.2369 | 0.1006 |
| P5 | 276.4 | -0.9217 | 0.1422 | 283.4 | -0.9195 | 0.1512 | 291.3 | -0.917 | 0.1599 | 300.1 | -0.9142 | 0.1684 | 309.9 | -0.9112 | 0.1764 |
| P6 | 805.7 | -0.6076 | 7.758 | 823.7 | -0.6454 | 7.819 | 842.1 | -0.6828 | 7.88 | 861 | -0.72 | 7.94 | 880.5 | -0.7568 | 8 |
| P7 | 619.4 | 18.09 | 17.29 | 633.5 | 18.08 | 17.43 | 647.7 | 18.07 | 17.57 | 661.9 | 18.06 | 17.71 | 676 | 18.04 | 17.85 |

Table 2 Constant Values for 50 Pieces of $\mathrm{Cn}^{2}$

We determined the coefficients of the polynomials for every $\mathrm{Cn}^{2}$. For the calculation of $p(x)$, we need to know $C n^{2}$ and $L$. If we have these values, we can find the coefficient values of the polynomial from the table of Table 1 and Table 2.

In Fig. 11, we plot the graphs of the coefficients with respect to the changes in $\mathrm{Cn}^{2}$. We obtained 21 graphs for all coefficient values. In Fig. 11, first row refers to the coefficients of the polynomial modeling of $A$, i.e., refers to the coefficients $A-$ $p 1$ to $A-p 7$, similarly the second row refers to $B-p 1$ to $B-p 7$ and third row refers $C-p 1$ to $C-p 7$ respectively.


Figure 11 Polynomial Equation Coefficient Values to $\mathrm{Cn}^{2}$ Graphs.

### 2.6 Comparison MATLAB Model and Integral Form of Probability Density Function

Considering all these processes we can claim that our simple equation which is expressed in (2.15) can be used instead of the complex integral equation which is defined in (2.16). For this comparison, we wrote a MATLAB code where we calculate both equations and plot their graphs as in Fig. 12. It is shown in Fig. 12 that our model and the original equation fit to each other very well.


Figure 12 Comparison of Result

In Fig. 12, red line was obtained from MATLAB model. Blue line was obtained from integral equation. As we see, both lines nearly overlap to each other. That means we can use equation (2.16) instead of equation (2.15). The developed expression is in closed form and it can be evaluated more easily.

## CHAPTER 3

## Calculations of Functions

### 3.1 Cumulative Distribution Function (CDF)

The cumulative distribution function for the $\log$ normal distribution model is obtained by integrating the probability density function of the $\log$ normal model (Prob. $\left(x^{2}<x\right)$. We obtain probability density function from MATLAB model which is given by (2.16).

$$
\begin{equation*}
C D F=\int_{0}^{x} p(x) d x \tag{3.1}
\end{equation*}
$$

Using equation (2.16) we can calculate the cumulative density function as in (3.2).

$$
\begin{equation*}
C D F=\int_{0}^{x} A \exp -\left(\frac{X-B}{C}\right)^{2} d x \tag{3.2}
\end{equation*}
$$

The error function is defined as in (3.3)

$$
\begin{equation*}
\emptyset(u)=\operatorname{erf}(u)=\frac{2}{\pi} \int_{0}^{u} e^{-x^{2}} d x \tag{3.3}
\end{equation*}
$$

We employ the error function in (3.3) for the pdf expression in (2.15) For this purpose, we write $U$ instead of $X$ as defined in equation (3.4) and after that we make some transformation for simple calculation of error function as in (3.5).

$$
\begin{equation*}
C D F=\int_{0}^{x} A \exp -\left(\frac{U-B}{C}\right)^{2} d u . \tag{3.4}
\end{equation*}
$$

$$
\begin{equation*}
y=(U-B) / C \quad d y=\left(\frac{1}{c}\right) d u \tag{3.5}
\end{equation*}
$$

After transformation of the cumulative distribution function we obtain a simpler equation as shown in (3.6). The defined limit of integral is divided into two parts as shown in equation (3.7).

$$
\begin{gather*}
C D F=\int_{-\frac{B}{C}}^{\frac{x-B}{C}} A e^{-y^{2}} C d y  \tag{3.6}\\
C D F=A C\left[\int_{\left(-\frac{B}{C}\right)}^{0} e^{-y^{2}} d y+\int_{0}^{\frac{x-B}{C}} e^{-y^{2}} d y\right] \tag{3.7}
\end{gather*}
$$

### 3.2 Moment Generating Function (MGF)

The $n$ degree moment of a random variable $X$ is defined as $E\left[X^{n}\right]$. For example, the first moment is the expected value $E[X]$. The second central moment is the variance of $X$. Similar to mean and variance, other moments give useful information about random variables. The moment generating function (MGF) of a random variable $X$ is a function $M_{X}(s)$ defined as

$$
\begin{equation*}
M_{x}(s)=E\left(e^{s x}\right)=\int_{0}^{\infty} P(x) e^{s x} d x \tag{3.8}
\end{equation*}
$$

and for our proposed model, the moment generating function is calculated as

$$
\begin{equation*}
M_{x}(s)=A e^{-\left(\frac{B^{2}}{C^{2}}\right)} \int_{0}^{\infty} e^{\left(\left(-\frac{x^{2}}{C^{2}}\right)+x\left(\left(\frac{2 B}{C^{2}}\right)+s\right)\right)} d x \tag{3.9}
\end{equation*}
$$

Which can be expressed in closed form using the $\phi(\cdot)$ function defined in [7, Eq. (3.322.2)] as

$$
\begin{equation*}
M_{x}(s)=A e^{-\left(\frac{B^{2}}{\left(C^{2}\right.}\right)} \sqrt{\left(\frac{\pi C^{2}}{4}\right)} \exp \left(-\left(\frac{C^{2}}{4}\right)\right)\left(\left(\frac{2 B}{C^{2}}\right)+S\right)^{2}\left[1-\emptyset-\left(\left(\frac{2 B}{C^{2}}\right)+S\right) \sqrt{\frac{C^{2}}{4}}\right] \tag{3.10}
\end{equation*}
$$

### 3.3 Moments

The "moments" of a random variable (or of its distribution) are expected values of powers or related functions of the random variable. Moments of the two signals for $\log$ normal distribution are calculated in equation (3.11),(3.12), (3.13) and (3.14).

$$
\begin{equation*}
E\left(X^{n}\right)=\left.\frac{d^{n}}{d s^{n}} M(s)\right|_{s=0} \tag{3.11}
\end{equation*}
$$

$$
\begin{equation*}
\emptyset\left(-\left(\frac{2 B}{c^{2}}+S\right)\right) \frac{C}{2}=\frac{2}{\sqrt{\pi}} \int_{0}^{\left(-\left(\frac{2 B}{c^{2}}+S\right)\right) \frac{C}{2}} e^{-x^{2}} d x \tag{3.12}
\end{equation*}
$$

$$
\begin{equation*}
\frac{d}{d s}\left(\frac{2}{\sqrt{\pi}} \int_{0}^{\left(-\left(\frac{2 B}{C^{2}}+s\right)\right) \frac{C}{2}} e^{-x^{2}} d x\right)=-\frac{2}{\sqrt{\pi}} e^{\left(-\left(\frac{2 B}{c^{2}}+S\right)^{2}\right) \frac{c^{2}}{4}} \frac{C}{2} \tag{3.13}
\end{equation*}
$$

$$
\begin{equation*}
\left.\frac{d M(s)}{d s}\right|_{s=0}=A e^{-\frac{B^{2}}{C^{2}}} \frac{\sqrt{\pi c^{2}}}{4}\left[\exp \left(\frac{B^{2}}{C^{2}}\right) B\right]\left[1-\emptyset\left(-\frac{B}{C}\right)\right]+\exp \left(\frac{B^{2}}{C^{2}}\right)\left(\frac{2}{\sqrt{\pi}} \frac{C}{2} e^{-\frac{B^{2}}{C^{2}}}\right) \tag{3.14}
\end{equation*}
$$

### 3.4 Outage Probability

The outage probability is defined as the probability that the SNR at the input of the receiver chain is falling below a given threshold value. Outage probability of our model is calculated in equation (3.15) and (3.16) .

$$
\begin{equation*}
P_{\gamma}=2 P(2 x) \quad P(x)=A \exp \left(-(x-B) / C^{2}\right) \tag{3.15}
\end{equation*}
$$

$$
\begin{equation*}
P_{\gamma}=2 A \exp \left(-(2 x-B) / C^{2}\right) \tag{3.16}
\end{equation*}
$$

### 3.5 Amount of Fading

The amount of fading is an important measure for severity of fading and it is defined as [10, Eq. (2.5)]

$$
\begin{equation*}
A F=\frac{\left(E\left(\tau^{2}\right)-(E(\tau))^{2}\right)}{E\left(\tau^{2}\right)} \tag{3.17}
\end{equation*}
$$

For the calculation of (3.17), we first compute $E\left(\tau^{2}\right)$ as outlined in (3.19), (3.20) and (3.21).

$$
\begin{equation*}
E\left(\tau^{2}\right)=\int_{0}^{\infty} \tau^{2} P(\tau) d \tau \rightarrow P(\tau)=A * \exp \left(-\left(\frac{(\tau-B)}{C}\right)^{2}\right) \tag{3.18}
\end{equation*}
$$

$$
\begin{equation*}
k=\frac{(\tau-B)}{C} \rightarrow \tau=C k+B \rightarrow d \tau=C d k \tag{3.19}
\end{equation*}
$$

$$
\begin{equation*}
E\left(\tau^{2}\right)=\int_{0}^{\infty} A C^{3} k^{2} e^{-k^{2}} d k+\int_{0}^{\infty} 2 A B C^{2} k e^{-k^{2}} d k+\int_{0}^{\infty} A B^{2} C e^{-k^{2}} d k \tag{3.21}
\end{equation*}
$$

$$
\stackrel{\Leftrightarrow}{\omega} \quad \stackrel{\leftrightarrow}{x} \quad \stackrel{\Theta}{Y}
$$

$$
\begin{equation*}
E\left(\tau^{2}\right)=\int_{-\infty}^{\infty} e^{-x^{2}} \sqrt{2} d x=\sqrt{2 \pi} \rightarrow \int_{-\infty}^{\infty} e^{-x^{2}} d x=\sqrt{\pi} \tag{3.23}
\end{equation*}
$$

$$
\begin{equation*}
\int_{-\infty}^{\infty} e^{-\frac{\tau^{2}}{2}} d y=\sqrt{2 \pi} \quad \rightarrow-\frac{\tau^{2}}{2}=x^{2} \rightarrow x=\frac{\tau}{\sqrt{2}} \quad \rightarrow d x=1 / \sqrt{2} d \tau \tag{3.22}
\end{equation*}
$$

Integration by parts is a technique for performing indefinite integration $\int u d v$ or definite integration

$$
\int_{a}^{b} u d v
$$

by expanding the differential of a product of functions $d(u, v)$ and expressing the original integral in terms of a known integral $\int v d u$. We made this transformation in equation (3.25) and (3.27).

For the $W$ part of equation (3.21), we have

$$
\begin{equation*}
\int_{0}^{\infty} A C^{3} k^{2} e^{-k^{2}} d k=A B^{2} C \sqrt{\pi} \tag{3.24}
\end{equation*}
$$

For the $X$ part of equation (3.21),

$$
\begin{equation*}
\int_{0}^{\infty} 2 A B C^{2} k e^{-k^{2}} d k \rightarrow-k^{2}=u \quad d u=-2 k d k \tag{3.25}
\end{equation*}
$$

$$
\begin{equation*}
-\int_{0}^{\infty} A B C^{2} e^{-u} d u=-A B C^{2} e^{-\left(\frac{(\tau-B)}{C}\right)^{2}} \tag{3.26}
\end{equation*}
$$

For the $Y$ part of equation (3.21), we have

$$
\begin{gather*}
\int_{0}^{\infty} A C^{3} k^{2} e^{-k^{2}} d k \rightarrow k^{2}=u \rightarrow k=\sqrt{u} \rightarrow d u=2 k d k \rightarrow e^{-k^{2}} d k=d v  \tag{3.27}\\
\rightarrow v=\sqrt{\pi} \\
\int_{0}^{\infty} \frac{1}{2 k} A C^{3} u e^{-u} d u=k^{2} \sqrt{\pi}-\int_{0}^{\infty} 2 \sqrt{\pi} k d k=0 \tag{3.28}
\end{gather*}
$$

At the end of transformation and calculation we can calculate $E\left(\tau^{2}\right)$ as shown in(3.29).

$$
\begin{equation*}
E\left(\tau^{2}\right)=A B^{2} C \sqrt{\pi}-A B C^{2} e^{-\left(\frac{\tau-B}{C}\right)} \tag{3.29}
\end{equation*}
$$

Second, we calculate $E(\tau)$ for the amount of fading as in equation (3.31), (3.32),(3.33),(3.34).

$$
\begin{equation*}
E(\tau)=\int_{0}^{\infty} \tau A e^{-\left(\frac{\sqrt{\tau}-B}{C}\right)^{2}} \tag{3.30}
\end{equation*}
$$

$$
\begin{equation*}
E(\tau)=\int_{0}^{\infty}\left(C^{2} k^{2}+2 B C k+B^{2}\right) A e^{-k^{2}}\left(2 C^{2} k+2 B C\right) d k \tag{3.31}
\end{equation*}
$$

$$
\begin{equation*}
\left(\frac{\sqrt{\tau}-B}{C}\right)=k \quad \rightarrow \tau=C^{2} k^{2}+2 B C k+B^{2} \rightarrow d \tau=2 C^{2} k+2 B C d k \tag{3.32}
\end{equation*}
$$

$E(\tau)=\int_{0}^{\infty} 2 A C^{4} k^{3} e^{-k^{2}} d k+\int_{0}^{\infty} 2 A C^{4} k^{3} e^{-k^{2}} d k+\int_{0}^{\infty} 2 A C^{4} k^{3} e^{-k^{2}} d k+\int_{0}^{\infty} 2 A C^{4} k^{3} e^{-k^{2}} d k$
A
B
C
D

For the $A$ part of equation (3.33),

$$
\begin{equation*}
\int_{0}^{\infty} 2 A C^{4} k^{3} e^{-k^{2}} d k=0 \tag{3.34}
\end{equation*}
$$

For the $B$ part of equation (3.33),

$$
\begin{equation*}
\int_{0}^{\infty} 6 A B C^{3} k^{2} e^{-k^{2}} d k=0 \tag{3.35}
\end{equation*}
$$

For the $C$ part of equation (3.33), we have

$$
\begin{equation*}
\int_{0}^{\infty} 6 A B^{2} C^{2} k e^{-k^{2}} d k=-3 A B^{2} C^{2} e^{-\left(\frac{\tau-B}{C}\right)^{2}} \tag{3.36}
\end{equation*}
$$

For the $D$ part of equation (3.33),

$$
\begin{equation*}
\int_{0}^{\infty} 2 A B^{3} C e^{-k^{2}} d k=2 A B^{3} C \sqrt{\pi} \tag{3.37}
\end{equation*}
$$

At the end of the all calculation $E(\tau)$ is equal to,

$$
\begin{equation*}
E(\tau)=2 A B^{3} C \sqrt{\pi}-3 A B^{2} C^{2} e^{-\left(\frac{\tau-B}{C}\right)^{2}} \tag{3.38}
\end{equation*}
$$

Now, we have all parameters to calculate the amount of fading which is expressed in (3.17). If we apply our calculated parameters to formula (3.17), amount of fading formula becomes as in (3.39).

$$
\begin{equation*}
A F=\frac{\left[A B^{2} C \sqrt{\pi}-A B C^{2} e^{-\left(\frac{\tau-B}{C}\right)}\right]-\left[2 A B^{3} C \sqrt{\pi}-3 A B^{2} C^{2} e^{-\left(\frac{\tau-B}{C}\right)^{2}}\right]}{\left[2 A B^{3} C \sqrt{\pi}-3 A B^{2} C^{2} e^{-\left(\frac{\tau-B}{C}\right)^{2}}\right]} \tag{3.39}
\end{equation*}
$$

### 3.6 Probability of Transmission Error Rate

In the last stage of thesis work, we calculate the probability of transmission error rate performance of the log-normal channels using our model. The modeling of the probability density function is done with $\bar{\mu}=15$. Now we consider the values of $\bar{\mu}$ from 5 up to 40 with incremental amount of 5 . We perform the same steps until Fig. 7. We calculate $p(x)$ of the harmonic mean and we plot its graph. Then, using MATLAB, we model the change of coefficients $A, B, C$ for all $\bar{\mu}$ values. We plot the graphs of $A, B, C$ coefficients with respect to $L$. Then, we use curve fitting option of MATLAB again and calculate polynomial coefficient for these graphs. The best fitting curve is achieved using a $6^{\text {th }}$ degree polynomial. Polynomial equations of $A, B, C$ graphs become as in (3.39) after fitting operation.

$$
\begin{equation*}
p_{1} X^{6}+p_{2} X^{5}+p_{3} X^{4}+p_{4} X^{3}+p_{5} X^{2}+p_{6} X^{1}+p_{7} \tag{3.39}
\end{equation*}
$$

This is a general polynomial equation with constant coefficients. We obtain these equations for each $\bar{\mu}$ value. Subsequently, we compare the models which are expressed by equation (2.15) and (2.16). We plot graphs for both equations with different $\bar{\mu}$ values on the same figure. Blue line is obtained from integral equation and red line is generated from our model.

For $\bar{\mu}=5$, coefficients of polynomial equations are given in (3.42). Graphs of $A, B$ and $C$ coefficents with respect to length are depicted in Fig. 13, 14 and 15. We plot the pdf obtained using the numerical integration and the one obtained using the modeling technique presented in this thesis work for $\bar{\mu}=5$ in Fig. 16.

$$
p 1 X^{6}+p 2 X^{5}+p 3 X^{4}+p 4 X^{3}+p 5 X^{2}+p 6 X^{1}+p 7
$$

| A | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | -0.1913 | -0.5432 | 3.294 | 17.11 | 33.33 | 38.05 | 23.5 |
| B | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | 0.00034 | 0.03009 | 0.01087 | -0.278 | 0.088 | 1.312 | 8.45 |
| C | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | 0.00996 | 0.02523 | -0.0743 | -0.159 | 0.369 | 5.539 | 12.0 |



Figure 13 Change of $A$ with respect to $L$ for $\bar{\mu}=5$


Figure 14 Change of $B$ with respect to $L$ for $\bar{\mu}=5$


Figure 15 Change of $C$ with respect to $L$ for $\bar{\mu}=5$


Figure 16 Comparisons of Results for $\bar{\mu}=5$

For $\bar{\mu}=10$, coefficients of polynomial equations are given in (3.43). Graphs of $A$, $B$ and $C$ coefficents with respect to length are depicted in Fig. 17, 18 and 19. We plot the pdf obtained using the numerical integration and the one obtained using the modeling technique presented in this thesis work for $\bar{\mu}=10$ in Fig. 20.

$$
p 1 X^{6}+p 2 X^{5}+p 3 X^{4}+p 4 X^{3}+p 5 X^{2}+p 6 X^{1}+p 7
$$

| A | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.5269 | -1.274 | -2.794 | 23.59 | 79.26 | 110.5 | 72.91 |
| B | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | -0.0099 | 0.0334 | 0.0736 | -0.297 | -0.150 | 0.985 | 13.27 |
| C | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | -0.0017 | 0.0184 | 0.0117 | -0.123 | 0.1307 | 5.432 | 12.2 |



Figure 17 Change of $A$ with respect to $L$ for $\bar{\mu}=10$


Figure 18 Change of $B$ with respect to $L$ for $\bar{\mu}=10$


Figure 19 Change of $C$ with respect to $L$ for $\bar{\mu}=10$


Figure 18 Comparisons of Results for $\bar{\mu}=10$

For $\bar{\mu}=15$, coefficients of polynomial equations are given in (3.44). Graphs of $A$, $B$ and $C$ coefficents with respect to length are depicted in Fig. 21, 22 and 23. We plot the pdf obtained using the numerical integration and the one obtained using the modeling technique presented in this thesis work for $\bar{\mu}=15$ in Fig. 24.

$$
p 1 X^{6}+p 2 X^{5}+p 3 X^{4}+p 4 X^{3}+p 5 X^{2}+p 6 X^{1}+p 7
$$




Figure 19 Change of $A$ with respect to $L$ for $\bar{\mu}=15$


Figure 20 Change of $B$ with respect to $L$ for $\bar{\mu}=15$


Figure 21 Change of $C$ with respect to $L$ for $\bar{\mu}=15$


Figure 22 Comparisons of Results for $\bar{\mu}=15$

For $\bar{\mu}=20$, coefficients of polynomial equations are given in (3.45). Graphs of $A$, $B$ and $C$ coefficents with respect to length are depicted in Fig. 25, 26 and 27. We plot the pdf obtained using the numerical integration and the one obtained using the modeling technique presented in this thesis work for $\bar{\mu}=20$ in Fig. 28 .

$$
p 1 X^{6}+p 2 X^{5}+p 3 X^{4}+p 4 X^{3}+p 5 X^{2}+p 6 X^{1}+p 7
$$

| A | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.8672 | 9.388 | -7.229 | -50.57 | 144.6 | 614.3 | 601.7 |
| B | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | -0.0177 | -0.008 | 0.149 | -0.080 | -0.5987 | -0.110 | 22.74 |
| C | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | -0.0043 | -0.008 | 0.0380 | 0.0259 | 0.0389 | 5.059 | 12.03 |



Figure 23 Change of $A$ with respect to $L$ for $\bar{\mu}=20$


Figure 24 Change of $B$ with respect to $L$ for $\bar{\mu}=20$


Figure 25 Change of $C$ with respect to $L$ for $\bar{\mu}=20$


Figure 26 Comparisons of Results for $\overline{\boldsymbol{\mu}}=\mathbf{2 0}$

For $\bar{\mu}=25$, coefficients of polynomial equations are given in (3.46). Graphs of $A$, $B$ and $C$ coefficents with respect to length are depicted in Fig. 29, 30 and 31. We plot the pdf obtained using the numerical integration and the one obtained using the modeling technique presented in this thesis work for $\bar{\mu}=25$ in Fig.32.

$$
p 1 X^{6}+p 2 X^{5}+p 3 X^{4}+p 4 X^{3}+p 5 X^{2}+p 6 X^{1}+p 7
$$

| A | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | -7.749 | 11.57 | 61.63 | -90.19 | -68.04 | 1020 | 1483 |
| B | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | 0.0010 | -0.0298 | 0.0506 | 0.0608 | -0.548 | -0.821 | 27.15 |
| C | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | 0.0070 | -0.0185 | -0.031 | 0.1034 | 0.180 | 4.813 | 11.75 |



Figure 27 Change of $A$ with respect to $L$ for $\bar{\mu}=25$


Figure 28 Change of $B$ with respect to $L$ for $\bar{\mu}=25$


Figure 29 Change of $C$ with respect to $L$ for $\bar{\mu}=25$


Figure 30 Comparisons of Results for $\bar{\mu}=25$

For $\bar{\mu}=30$, coefficients of polynomial equations are given in (3.47). Graphs of $A$, $B$ and C coefficents with respect to length are depicted in Fig. 33, 34 and 35. We plot the pdf obtained using the numerical integration and the one obtained using the modeling technique presented in this thesis work for $\bar{\mu}=30$ in Fig. 36 .

$$
p 1 X^{6}+p 2 X^{5}+p 3 X^{4}+p 4 X^{3}+p 5 X^{2}+p 6 X^{1}+p 7
$$

| A | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | -0.8659 | -21.56 | 80.18 | 89.19 | -410.4 | 1103 | 3078 |
| B | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | 0.01401 | -0.023 | -0.056 | 0.1009 | -0.3466 | -1.52 | 31.24 |
| C | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | 0.00560 | -0.018 | -0.039 | 0.1423 | 0.2551 | 4.585 | 11.43 |



Figure 31 Change of $A$ with respect to $L$ for $\bar{\mu}=30$


Figure 32 Change of $B$ with respect to $L$ for $\bar{\mu}=30$


Figure 33 Change of $C$ with respect to $L$ for $\bar{\mu}=30$


Figure 34 Comparisons of Results for $\bar{\mu}=30$

For $\bar{\mu}=35$, coefficients of polynomial equations are given in (3.48). Graphs of $A$, $B$ and $C$ coefficients with respect to length are depicted in Fig. 37, 38 and 39. We plot the pdf obtained using the numerical integration and the one obtained using the modeling technique presented in this thesis work for $\bar{\mu}=35$ in Fig. 40 .

$$
p 1 X^{6}+p 2 X^{5}+p 3 X^{4}+p 4 X^{3}+p 5 X^{2}+p 6 X^{1}+p 7
$$

| A | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 25.87 | -25.26 | -110 | 342.9 | -318.1 | 549.9 | 5111 |
| B | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | 0.0021 | 0.0026 | -0.050 | 0.0310 | -0.1771 | -2.129 | 34.98 |
| C | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | -0.0022 | -0.011 | -0.010 | 0.1516 | 0.2688 | 4.36 | 11.14 |



Figure 35 Change of A with respect to L for $\bar{\mu}=35$


Figure 36 Change of B with respect to L for $\bar{\mu}=35$


Figure 37 Change of C with respect to L for $\bar{\mu}=35$


Figure 38 Comparisons of Results for $\bar{\mu}=35$

For $\bar{\mu}=40$, coefficients of polynomial equations are given in (3.49). Graphs of $A$, $B$ and $C$ coefficients with respect to length are depicted in Fig. 41, 42 and 43. We plot the pdf obtained using the numerical integration and the one obtained using the modeling technique presented in this thesis work for $\bar{\mu}=40$ in Fig. 44 .

$$
p 1 X^{6}+p 2 X^{5}+p 3 X^{4}+p 4 X^{3}+p 5 X^{2}+p 6 X^{1}+p 7
$$

| A | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | -16.04 | 50.97 | -19.14 | 88.65 | 53.49 | 144.3 | 6533 |
| B | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | -0.0075 | 0.0097 | -0.005 | -0.040 | -0.030 | -2.71 | 38.42 |
| C | P 1 | P 2 | P 3 | P 4 | P 5 | P 6 | P 7 |
|  | -0.005 | -0.0063 | 0.010 | 0.146 | 0.2789 | 4.122 | 10.89 |



Figure 39 Change of A with respect to L for $\bar{\mu}=40$


Figure 40 Change of B with respect to L for $\bar{\mu}=40$


Figure 41 Change of C with respect to L for $\bar{\mu}=40$


Figure 42 Comparisons of Results for $\bar{\mu}=40$

### 3.7 Average Probability of Transmission Error Rate

In this section, we calculate $A, B$ and $C$ coefficient values for $8 \bar{\mu}$ values ranging from 0 to 40 . For the calculation of coefficient values we use MATLAB curve fitting option for $p(x)$ equation which is defined in expression (2.16). Coefficient values are tabulated in Fig. 45.

| $\bar{\mu}$ | A | B | C |
| :--- | :--- | :--- | :--- |
| $\bar{\mu}=5$ | 10,96 | 7,835 | 9,283 |
| $\bar{\mu}=10$ | 33,64 | 12,76 | 9,425 |
| $\bar{\mu}=15$ | 105,7 | 17,73 | 9,46 |
| $\bar{\mu}=20$ | 326,9 | 22,66 | 9,414 |
| $\bar{\mu}=25$ | 951,2 | 27,44 | 9,284 |
| $\bar{\mu}=30$ | 2393 | 31,92 | 9,098 |
| $\bar{\mu}=35$ | 4680 | 36,03 | 8,925 |
| $\bar{\mu}=40$ | 6459 | 39,82 | 8,803 |

Table 3 List of Coefficients for Different $\bar{\mu}$ Values

After calculation of coefficient values, we compute probability of average transmission error with respect to average signal to noise ratio (SNR). We use the equation in (3.50) to calculate $P_{e}$ values

$$
\begin{equation*}
P_{e}=\left(\frac{1}{\pi} \int_{0}^{\frac{\pi}{2}} M_{s}\left(\frac{\Psi}{\sin ^{2} \theta}\right) d \theta\right) \tag{3.50}
\end{equation*}
$$

In (3.50) $M_{s}$ represents the moment generating function defined in (3.8). We assign $\sin ^{2} \theta=S, \Psi=1 / 2$. After these assignments equation (3.50) becomes as in (3.51).

$$
\begin{equation*}
P_{e}=\left(\frac{1}{\pi} \int_{0}^{\frac{\pi}{2}} M_{s}\left(\frac{1}{2 S}\right) d s\right) \tag{3.51}
\end{equation*}
$$

We calculate all $P_{e}$ values with respect to SNR ranging from 0 to 40 in steps of 5 . We plot transmission error probability $P_{e}$ with respect to Signal to noise ratio (SNR) in Fig. 45.


Figure 43 Average Probability of Transmission Error Rate to SNR

From this Fig. 45, it is obvious that as the average SNR increases, probability of transmission error decreases rapidly. Thus for $\bar{\mu}=40 \mathrm{~dB}$ the probability of transmission error is less than $10^{-12}$

## CHAPTER 4

## CONCLUSION

In this thesis study, we demonstrated how to develop a mathematical model in closed form for those systems having performance expressions in numerical integration form. For this purpose, we considered two-hop communication systems whose end-to-end performance depends on the harmonic mean of the hop SNRs. We considered two-hop systems with log-normally distributed optical communication channels. We derived an expression for the harmonic mean of two-hop systems employing lognormally distributed channels. Later, for the derived expression, using the curve fitting utility of the MATLAB compiler, we developed a simple Gaussian like expression for the derived harmonic mean expression, and using the developed approximate expression we calculated the cumulative distribution function, moment generating function, and transmission error probability, for two-hop communication systems with log-normal channels.

FSO offers many advantages over existing techniques which can be either optical or radio or microwave. Less cost and time to setup are the main attraction of FSO system. Optical equipment can be used in FSO system with some modification. Merits of FSO communication system and its application area make it a hot technology but there are some problems arising due to the attenuation caused by medium. FSO system poses some problem like attenuation in medium that can affect the performance of transmission as power loss would be there. But extra care and restudy of the medium can guide what type of parameters to be considered before setting up the system.

In this work, we have derived closed-form expression for the evaluation of the average capacity and the outage probability of a typical two-hop FSO
communication system over turbulence atmospheric conditions modeled by log normal distribution respectively. We studied the dependence of the reliability and the performance of a system as a function of the principal parameters of such a link, being the length of the link, aperture diameter of the receiver and the atmospheric turbulence conditions between transmitter and receiver. If we know the value of length between transmitter and receiver and turbulence strength according to atmospheric conditions, we can calculate performance of channels easily thanks to our model which is explained in this thesis.

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## APPENDICES A CURRICULUM VITAE

## PERSONAL INFORMATION

Surname, Name: Görse, Serkan
Date and Place of Birth: 20 February 1989, Ankara
Marital Status: Single
Phone: +90 5385455320
Email: gorse.serkan@gmail.com

## EDUCATION

Degree
B.Sc.

High School

## Institution

Cankaya Univ., Electronic and
Communication Engineering
Inonu High School 2006

WORK EXPERIENCE

| Year | Place | Enrollment |
| :--- | :--- | :--- |
| High Speed Trains |  |  |
| 2016-Present |  | Signalization System Chief |
| $2015-2016$ | THALES | Engineer |
| $2013-2015$ |  | Medical Devices Supervisor |
|  | Groland Group | R\&D Engineer |

## PROJECTS

May 2016 -
Present

Company: THALES
Department: Technical Department of Maintenance Project Definition: My responsibilities are stated below in this position;

1-Communicating with TCDD site staff about maintenance problems regularly for progress payment.

2-Fulfillment of the duties of maintenance department
3-Control of version, application and updates
4-Monitoring and control of the situation and reporting
5-Preventive Maintenance Activity
6-Troubleshooting and Corrective Maintenance Activity
7-Reporting failure statistics monthly and yearly.

April 2016 - Company: Altay Kollektif
May 2016 Department: MGEO Aselsan Team
Project Definition: Producing embedded test software for unmanned aerial vehicle which name is ANKA. In this project I am producing some embedded software in $\mathrm{C}++$ for making functionality tests of ANKA.

October 2015- Company: Proland Group
April 2016 Department: Medical Devices Department Project Definition: I was designing embedded software for medical devices and I was coordinating production of these devices for all hospitals in Turkey.

August 2014- Company: GATE Electronic Inc.
February 2015 Department: Communication-Electronics Systems Team Project Name: PXI - DAQ Data Acquisition Card

Project Definition: I was designing embedded software for an FPGA module and PCB. While I was designing PCB card and embedded software I used Altium Designer and MPLAB packet programs.

August 2014- Company: GATE Electronic Inc.
October 2015 Department: Communication-Electronics Systems Team Project Name: DSBCA

Project Definition: In this project I produce a program for testing electronic card which are using in Cougar Helicopters using by Turkish air forces.

April 2013- Company: GATE Electronic Inc.
November 2014 Department: Communication-Electronics Systems Team
Project Name: Portable Jammer Tester
Project Definition: In this project I produce an embedded program and a PCB card for testing Jammers which are using in Turkish army. Thanks to this device soldiers can test their jammers while they are on the area

April 2013- Company: GATE Electronic Inc.
August 2014 Department: Communication-Electronics Systems Team Project Name: GATESEM

Project Definition: In this project I produce an embedded program which is integrated with walkie-talkie using by police forces. Thanks to this program police forces communicate with an encryption algorithm.

## HOBBIES

Travelling, Football, Basketball, Cinema

